The Exchange of $H_2^{18}O$ with the Oxygen of Promoters on the Surface of Iron Catalysts

V. SOLBAKKEN,* Å. SOLBAKKEN,* AND P. H. EMMETT

Department of Chemistry, The Johns Hopkins University, Baltimore, Maryland 21218

Received February 28, 1969; revised April 7, 1969

The oxygen content of promoter oxides or other metallic oxide on the surface of iron synthetic ammonia catalysts has been estimated by a method involving equilibration with a known quantity of $H_2^{15}O$ in hydrogen at 450°C. The results indicate a surface coverage by promoters of about 60% for a catalyst containing 1.06% Al₂O₃ and 0.52% K₂O. With reasonable assumptions in regard to the cross sectional area of oxygen ions the coverage agrees with that estimated from the chemisorption of carbon monoxide at -195°C on the same catalyst. A pure iron catalyst revealed only a 1.2% coverage with oxygen after extended reduction at 450°C.

INTRODUCTION

Iron synthetic ammonia catalysts are commonly promoted with small amounts of alkaline oxides or alkaline earth oxides such as K_2O , CaO, or MgO, together with a few percent of an irreducible oxide such as Al_2O_3 or SiO_2 . Several approaches have been used in an effort to ascertain the fraction of the surface of the reduced catalysts actually covered by the few percent added promoter. Emmett and Brunauer (1, 2) showed that the chemisorption of carbon monoxide at -195 or -183° C will cover the entire surface of a pure iron catalyst but only about 40% of the surface of a catalyst containing 1 or 2% of a $K_2O-Al_2O_3$ promoter. Furthermore, they showed that the $K_2O-Al_2O_3$ promoter, itself, was capable of chemisorbing an amount of carbon dioxide at -78° equivalent to about 60% of the surface of the entire catalyst. These facts combined with the inability of a pure iron catalyst to adsorb any carbon dioxide at -78° led to the conclusion that a few percent promoter in these iron catalysts would cover 50-70% of the surface leaving

* Present address: Institute of Industrial Chemistry, The Technical University of Norway, Trondheim, Norway. only 30-50% of the surface in the form of iron. Scholten (3) discussed the method used by Emmett and Brunauer and pointed out that their procedure for determining the amount of chemisorption by obtaining data for an adsorption isotherm at -195° , evacuating the sample at -78° , and then measuring again the adsorption at -195° might be somewhat in error because of the possibility that some of the chemisorption might pump off at -78°C. As an alternate procedure they measured the exchange of D_2O with the remaining OH groups on the Al_2O_3 of the iron catalyst and compared the amount of exchange with that occurring on a sample of Al₂O₃ of known area pretreated with hydrogen at 450°C, the temperature used for the reduction of the iron catalyst. By assuming that the exchange per unit area covered by Al_2O_3 as a promoter on the surface of the iron would be the same as on the Al_2O_3 sample they were able to estimate the fraction of the surface of the iron catalyst covered by promoter. This method suggested that 1% Al_2O_3 as a promoter covered about 25% of the surface leaving 75% as the free iron surface. For such a catalyst the method of Emmett and Brunauer indicated that 45% of the surface was iron and 55% was covered with aluminum oxide. In the present



FIG. 1. The equipment used for the exchange of $H_2^{18}O$ with ^{16}O in promoters on the surface of iron catalysts.

work an attempt has been made to obtain a third estimate of the fraction of the surface covered by promoter. This third method entails adding a mixture of $H_2^{18}O$ and hydrogen to the reduced catalyst and letting it stand until equilibrium is set up between the oxygen-16 in the promoter and oxygen-18 of the water vapor. The results of these measurements are reported in the present paper.

EXPERIMENTAL

The experimental set-up is illustrated in Fig. 1. The reactor (about 20 cc) was constructed so that it could be filled and emptied without getting air into the system. The catalyst, the amount of which was chosen so that the surface area was 5-7 m^2 , was introduced through a standard tapered joint at the top of the reactor while helium was streaming through. It could be emptied through a similar joint in the bottom of the reactor. The plug in the bottom supported a rod with a loosely fitting plunger to keep the catalyst in the reactor zone but to allow gas to stream by. Fitting a plastic bag filled with inert gas around the bottom plug helped in the removal of the highly active catalyst without getting it in contact with air.

A furnace around the reactor was controlled by a thyratron unit to a temperature of $450^{\circ}C \pm 1^{\circ}$ during reduction and exchange. The catalyst was reduced with 60 ml/min of hydrogen. During some experiments it was taken directly from the tank (Matheson "zero" gas, "analyzed") but during most of the experiments it was first allowed to diffuse through a palladiumsilver alloy tube. The reduction time was usually 18 hr but was extended in some instances for comparison to 42 and 114 hr. Some of the samples were subject to several successive exchanges with H₂¹⁸O to see whether the sublayers of oxygen also were exchanged. During these experiments the catalyst was always reduced 18 hr between each run. After the reduction, the sample was pumped for 30 min and a measured amount of water enriched with oxygen-18 was introduced into the reactor by first freezing it into a trap from the measuring system, and then melting and evaporating it into the reactor. The trap was flushed with hydrogen so the H_2 pressure in the reactor was about 300 mm Hg during the exchange. The water-hydrogen mixture was kept in contact with the catalyst for 3 hrs. In two experiments, 1 and 5 hr were used to be sure that equilibrium had been reached. The gas was then flushed into a $-195^{\circ}C$ trap (about 5 cc) with a stream of hydrogen which also reduced off any surface oxide. The reduction was continued for 30 min although times from 10 min to 5 hr were tried without changing the concentration of oxygen-18 in the water product, further evidence that equilibrium had been reached. The trap was connected through a stopcock to a Consolidated 21-611 mass spectrometer as shown in Fig. 1. The memory effect of the mass spectrometer could be overcome by introducing consecutively 10-15 samples $(0.025 \text{ cc } H_2O \text{ [S.T.P.] each})$ of the trapped water vapor. In between each introduction the expansion chamber and connecting tubes were briefly pumped for 3 min; usually five isotope measurements were made for each introduced sample. The values for each of these measurements were statistically treated to find the concentration at zero time. The results were highly reproducible.

The catalysts used in these experiments were the following: No. 418, a doubly promoted iron catalysts containing 1.06% Al_2O_3 and 0.52% K₂O (based on unreduced catalyst); No. 927, with no promoters added, but probably containing up to 0.15% Al_2O_3 as an impurity; and No. 954, a singly promoted catalyst containing 10.2% Al_2O_3 . In addition, S(Fe)1 was prepared as a porous pure iron catalyst made from pure chemicals after a method described by Emmett and Gray (4). To confirm that the exchange takes place only on the surface of the Al_2O_3 phase, two samples of alpha-alumina with a specific surface of 4.40 m^2/g were treated in exactly the same way as the iron catalyst samples and exchanged in the $H_2^{18}O-H_2$ mixture.

The surface area (5) and the CO chemisorption values were measured on a McBain type balance with a sensitivity such that the quartz spiral increased in length 1 mm for each 2 mg added weight. Samples weighing approximately 1 g were used. The extension of the spiral was read with a travelling microscope with a sensitivity of about 0.002 mm. The CO was adsorbed at -195.8° C at a few millimeters pressure and then pumped at the same temperature with an effective diffusion pump with large diameter tubes. A steady state was reached after 2.5-3 hr while pumping down to 10⁻⁶ mm Hg. The CO which did not come off after 4 hr pumping was assumed to be chemisorbed. Experiment M86 on catalyst No. 418 illustrated in Fig. 4 made it evident that this final value attained by pumping at -195° C was substantially the same as that obtained by a short pumping at -78°C.

RESULTS AND DISCUSSION

Figure 2 shows how the mass spectrometer readings came to a steady state after some 10–15 introductions of sample with a 3-min pumping in between. The last values were usually within a few tenths of a percent of each other. The scale on the left gives the percentage ¹⁸O measured



FIG. 2. Representative plots of the measured concentration of ¹⁸O in the sample as a function of n, the number of introductions of the sample into the mass spectrometer.

43 418 1.00 18 3 0.0659 45.5 0.0659 (7.04) ^a 0 44 Same 18 3 0.0661 63.5 (0.0835) 0 45 Same 18 3 0.0658 68.7 (0.1038) 0 46 Empty 18 3 0.0652 83.3 (0.0185) (1.98) ^a 0 47 S(Fe)1 5.11 42 3 0.0652 83.3 (0.0185) (1.98) ^a 0 48 Same 18 3 0.0652 44.8 0.0672 (7.04) ^a 0 50 418 1.00 18 5 0.0652 44.8 0.0672 (7.04) ^a 0 52 Same 18 0.0613 61.9 (0.0830) 6.54 0 54 418 1.00 42 3 0.0667 47.9 0.0600 6.40 0 55 Empty 18 3 0.0648 91.2 (0.0000) 1.98 0 56 S(Fe)	Run M No.	Cat.	Red. cat. (g)	Red. (hr)	Exch. (hr)	a ₀ mmole enriched H ₂ O added	x_1 % H ₂ ¹⁸ O in water after equil.	a _i Oxygen on surf. (matom)	Spec. surf. area (m²/g)	No. of O atoms per cm ² $ imes 10^{-15}$
44 Same 18 3 0.0661 63.5 (0.0835) 45 Same 18 3 0.0658 68.7 (0.1038) 46 Empty 18 3 0.0674 91.1 1 47 S(Fe)1 5.11 42 3 0.0655 82.5 0.0067 (1.98) ^a (0.48) ^a 48 Same 18 3 0.0652 83.3 (0.0185) (1.98) ^a (0.51) 49 Empty 18 3 0.06614 61.9 (0.0830) 6.54 50 418 1.00 18 1.00631 61.9 (0.0830) 6.54 51 418 1.00 42 3 0.0667 47.9 0.0600 6.40 0 55 Empty 18 3 0.0648 90.4 - - 56 S(Fe)1 2.16 42 3 0.0633 89.7 0.0000 1.98 58 927 7.43 42 3 0.0648 91.2 (0.0000) 1.98 58 927	43	418	1.00	18	3	0.0659	45.5	0.0659	(7.04) ^a	0.563
45 Same 18 3 0.0658 68.7 (0.1038) 46 Empty 18 3 0.0674 91.1 $(1.98)^a$ (0.1038) 47 S(Fe)1 5.11 42 3 0.0655 82.5 0.0067 $(1.98)^a$ $(0.138)^a$ 48 Same 18 3 0.0652 83.3 $(0.0185)^a$ $(1.98)^a$ $(0.138)^a$ 50 418 1.00 18 3 0.0652 44.8 0.0672 $(7.04)^a$ $(0.514)^a$ 50 418 1.00 18 1 0.0631 43.0^a 0.0704 $(7.04)^a$ $(0.514)^a$ 51 418 1.00 43 3 0.0667 47.9^a 0.0600^a 6.54^a 54 418 1.00^a 42 3 0.0667^a 47.9^a 0.0000^a $(1.98)^a$ 0^a 0^a 0^a 55 Empty 18 3 0.0661^a 87.2^a 0.58^a 0^a 0^a 0^a 0^a	44	Same		18	3	0.0661	63.5	(0.0835)		
46 Empty 18 3 0.0674 91.1 47 S(Fe)1 5.11 42 3 0.0655 82.5 0.0067 $(1.98)^a$ 0 48 Same 18 3 0.0652 83.3 (0.0185) $(1.98)^a$ 0 49 Empty 18 3 0.0662 44.8 0.0672 $(7.04)^a$ 0 50 418 1.00 18 1 0.0631 43.0 0.0704 $(7.04)^a$ 0 51 418 1.00 42 3 0.0667 47.9 0.0600 6.40 0 52 Same 18 3 0.0648 90.4 0.0500 6.40 0 55 Empty 18 3 0.0647 82.3 0.0009 $(1.98)^a$ 0 56 S(Fe)1 2.16 42.3 0.0647 82.3 0.0009 $(1.98)^a$ 0 57 Same 18 3 0.0647 82.3 0.0009 $(1.98)^a$ <td>45</td> <td>Same</td> <td></td> <td>18</td> <td>3</td> <td>0.0658</td> <td>68.7</td> <td>(0.1038)</td> <td></td> <td></td>	45	Same		18	3	0.0658	68.7	(0.1038)		
47 $S(Te)I$ 5.11 42 3 0.0655 82.5 0.0067 $(1.98)^a$ 0 48 Same 18 3 0.0652 83.3 (0.0185) $(1.98)^a$ 0 49 Empty 18 3 0.0652 83.3 (0.0185) $(1.98)^a$ 0 50 418 1.00 18 5 0.0652 44.8 0.0672 $(7.04)^a$ 0 51 418 1.00 18 1 0.0631 61.9 0.0704 $(7.04)^a$ 0 52 Same 18 3 0.0667 47.9 0.0600 6.40 0 55 Empty 18 3 0.0648 90.4 0 0 0 57 Same 18 3 0.0647 82.3 0.0009 $1.98)^a$ 0 58 927 7.43 42 3 0.0647 82.3 0.0068 $(0.66)^a$ 0 67 418 1.00 18 3 <	46	Empty		18	3	0.0674	91.1	. ,		
48 Same 18 3 0.0652 83.3 (0.0185) $(1.98)^a$ 49 Empty 18 3 0.0649 90.8 90.8 50 418 1.00 18 5 0.0652 44.8 0.0672 $(7.04)^a$ 0 51 418 1.00 18 3 0.0613 61.9 (0.0830) 6.54 52 Same 18 3 0.0667 47.9 0.0600 6.40 0 54 418 1.00 42 3 0.06673 89.7 0.0000 $(1.98)^a$ 0 55 Empty 18 3 0.0648 90.4 90.4 90.8 0 56 S(Fe)1 2.16 42 3 0.0647 82.3 0.0000 1.98^a 0 57 Same 18 3 0.0651 87.2 0.58 0 67 418 1.00 18 3 0.0612 91.6 0 70 418 1.00 <	47	S(Fe)1	5.11	42	3	0.0655	82.5	0.0067	$(1.98)^{a}$	0.040
49Empty183 0.0649 90.8 504181.00185 0.0652 44.8 0.0672 $(7.04)^a$ $(0.51)^a$ 514181.00181 0.0631 43.0 0.0704 $(7.04)^a$ $(0.52)^a$ 52Same183 0.0613 61.9 (0.0830) 6.54544181.00423 0.0667 47.9 0.0600 6.40 $(0.55)^a$ 55Empty183 0.0648 90.4 $(0.0000)^a$ $(1.98)^a$ $(0.57)^a$ 56S(Fe)12.16423 0.0647 82.3 0.0068 $(0.66)^a$ $(0.59)^a$ 57Same183 0.0651 87.2 0.58 $(0.66)^a$ $(0.58)^a$ $(0.66)^a$ $(0.58)^a$ 57Same183 0.0651 87.2 0.58 $(0.66)^a$ $(0.67)^a$ $(0.600)^a$ $(0.67)^a$ $(0.66)^a$ 59Same183 0.0612 91.6 $(0.700)^a$ 6.98^a $(0.67)^a$ $(0.77)^a$ $(0.77)^a)^a$ $(0.77)^a$ 67418 1.00 18 3 0.0610^a $(0.0700)^a$ 6.42^a $(0.77)^a$ $(0.67)^a$ $(0.67)^a$ $(0.67)^a$ $(0.67)^a$ $(0.67)^a$ $(0.67)^a$ $(0.67)^a$ $(0.67)^a$ $(0.66)^a$ $(0$	48	Same		18	3	0.0652	83.3	(0.0185)	$(1.98)^{a}$	
504181.001850.065244.80.0672 $(7.04)^{\circ}$ 0514181.001810.063143.00.0704 $(7.04)^{\circ}$ 052Same1830.061361.9 (0.0830) 6.54544181.004230.066747.90.06006.40055Empty1830.064890.456S(Fe)12.164230.065389.70.0009 $(1.98)^{\circ}$ 057Same1830.064891.2 (0.0000) 1.98589277.434230.065187.20.58674181.001830.065187.20.58674181.001830.061291.6704181.001830.061060.9 (0.0700) 6.427474Empty1830.061060.9 (0.0700) 6.427474Empty1830.065390.5754181.004230.055343.10.06146.550754181.001430.065947.70.0602(6.40)^{a}0764181.001430.065947.70.0602(6.40)^{a}079Same1830.065679.6 (0.0644) 8888	49	Empty		18	3	0.0649	90.8	• •		
51 418 1.00 18 1 0.0631 43.0 0.0704 $(7.04)^a$ 0 52 Same 18 3 0.0613 61.9 (0.0830) 6.54 54 418 1.00 42 3 0.0667 47.9 0.0600 6.40 0 55 Empty 18 3 0.0648 90.4	50	418	1.00	18	5	0.0652	44.8	0.0672	$(7.04)^{a}$	0.574
52 Same 18 3 0.0613 61.9 (0.0830) 6.54 54 418 1.00 42 3 0.0667 47.9 0.0600 6.40 0 55 Empty 18 3 0.0653 89.7 0.0009 (1.98) ^a 0 56 S(Fe)1 2.16 42 3 0.0648 91.2 (0.0000) 1.98 57 Same 18 3 0.0647 82.3 0.0068 (0.66) ^a 0 58 927 7.43 42 3 0.0651 87.2 0.58 0 67 418 1.00 18 3 0.0612 91.6 0 0 70 418 1.00 18 3 0.0610 60.9 (0.0700) 6.42 0 74 Empty 18 3 0.0653 49.3 0.0548 6.29 0 75 418 1.00 14 3 0.0654 68.6 (0.0647) 0 78 418 1.00	51	418	1.00	18	1	0.0631	43.0	0.0704	$(7.04)^{a}$	0.602
544181.004230.066747.90.06006.40055Empty1830.064890.4656 $S(Fe)1$ 2.164230.065389.70.0009 $(1.98)^a$ 057Same1830.064891.2 (0.0000) 1.980589277.434230.064782.30.0068 $(0.66)^a$ 059Same1830.065187.20.580674181.001830.055440.10.07036.98069Empty1830.061291.60704181.001830.061290.5074Empty1830.060790.50754181.004230.055343.10.06146.550764181.001430.065390.500077Empty1830.065448.6(0.0647)0784181.004230.065547.70.0602(6.40)^a079Same1830.065573.80.01560.660839277.434230.065573.80.01560.66084 $a -Alumina$ 0.6101830.065259.10.0352(4.39) </td <td>52</td> <td>Same</td> <td></td> <td>18</td> <td>3</td> <td>0.0613</td> <td>61.9</td> <td>(0.0830)</td> <td>6.54</td> <td></td>	52	Same		18	3	0.0613	61.9	(0.0830)	6.54	
55Empty183 0.0648 90.4 56S(Fe)12.16423 0.0653 89.7 0.0009 $(1.98)^a$ 0.657 57Same183 0.0648 91.2 (0.0000) 1.98 0.653 58 927 7.43423 0.0647 82.3 0.0068 $(0.66)^a$ 0.659^a 59Same183 0.0651 87.2 0.58 0.669^a 0.669^a 0.669^a 0.669^a 674181.00183 0.0612 91.6 0.703 6.98 0.669^a 0.6663 704181.00183 0.0611 91.6 0.7000 6.42^a 0.6663 $(7.04)^a$ 0.6663 71Same18 3 0.0610 60.9 (0.0700) 6.42^a 0.6614 6.55 0.6614 74Empty18 3 0.0653 90.5 0.6644 0.6644 0.6644 0.6644 74Empty18 3 0.0653 90.5 0.6644 0.6647 0.6644 0.6649^a 0.6644 75418 1.00 42 3 0.6656 79.6 (0.0664) 0.6644 0.6653 7.04 0.6644 81Same18 3 0.6655 73.8 0.0156 5.86 0.666 0.666 0.666 0.666 0.666 0.666 0.666 0.666 0.666 0.666 0.6660	54	418	1.00	42	3	0.0667	47.9	0.0600	6.40	0.564
56 $S(Fe)1$ 2.164230.0653 89.7 0.0009 $(1.98)^a$ 057Same1830.0648 91.2 (0.0000) 1.98 58 927 7.43423 0.0647 82.3 0.0068 $(0.66)^a$ 059Same183 0.0651 87.2 0.58 067418 1.00 183 0.0554 40.1 0.0703 6.98 069Empty183 0.0612 91.6 070418 1.00 183 0.0610 60.9 (0.0700) 6.42 74Empty183 0.0607 90.5 075418 1.00 423 0.0553 43.1 0.0614 6.55 076418 1.00 143 0.0648 49.3 0.0548 6.29 077Empty183 0.0653 90.5 0078418 1.00 423 0.0654 68.6 (0.0647) 80Same183 0.0655 45.6 0.0653 7.04 081Same183 0.0655 73.8 0.0156 7.04 083 927 7.43 42 3 0.0655 73.8 0.0156 0.666 084 $a-Alumina$ 0.610 18 3 0.0655 73.8 0.0156 6.66	55	Empty		18	3	0.0648	90.4			
57Same183 0.0648 91.2 (0.000) 1.98 58 927 7.43 42 3 0.0647 82.3 0.0068 $(0.66)^a$ $0.65)^a$ 59Same 18 3 0.0651 87.2 0.58 67 418 1.00 18 3 0.0554 40.1 0.0703 6.98 0.698 69Empty 18 3 0.0612 91.6 0.0703 6.98 0.698 70 418 1.00 18 3 0.0411 34.8 0.0663 $(7.04)^a$ 0.642 74Empty 18 3 0.0610 60.9 (0.0700) 6.42 0.744^a 0.753^a 74Empty 18 3 0.0653 43.1 0.0614 6.55^a 0.76^a 75 418 1.00 114 3 0.6648 49.3 0.0548 6.29^a 0.77^a 76 418 1.00 114 3 0.0653^a 90.5^a 0.77^a 0.6002^a $(6.40)^a$ 0.77^a 78 418 1.00 42^a 3 0.0656^a 79.6^a $(0.0647)^a$ 0.6669^a 5.86^a 82 418 1.00 18^a 3 0.0655^a 73.8^a 0.0156^a 0.66^a 83 927^a 7.43^a 42^a 3 0.0655^a 73.8^a 0.0156^a 0.66^a 83 $a-Alumina$ 0.610^a 18^a 3 0.06	56	S(Fe)1	2.16	42	3	0.0653	89.7	0.0009	(1.98) ^a	0.012
58 927 7.43 42 3 0.0647 82.3 0.0068 $(0.66)^a$ 0 59 Same 18 3 0.0651 87.2 0.58 0 67 418 1.00 18 3 0.0554 40.1 0.0703 6.98 0 69 Empty 18 3 0.0612 91.6 9 9 0 0 7 418 1.00 18 3 0.0610 60.9 (0.0700) 6.42 0 74 Empty 18 3 0.0607 90.5 9 7 7 18 1.00 14 3 0.0653 90.5 9 0 7 7 18 1.00 14 3 0.0653 90.5 9 0 7 7 18 1.00 14 3 0.0653 90.5 9 7 7 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10	57	Same		18	3	0.0648	91.2	(0.0000)	1.98	
59Same183 0.0651 87.2 0.58 67418 1.00 183 0.0554 40.1 0.0703 6.98 0.698 69Empty183 0.0612 91.6 0.0703 6.98 0.663 70418 1.00 183 0.0411 34.8 0.0663 $(7.04)^a$ 0.6703 71Same183 0.0610 60.9 (0.0700) 6.42 74Empty183 0.0607 90.5 0.614 6.55 0.663 75418 1.00 423 0.0653 90.5 0.0548 6.29 0.0770 76418 1.00 1143 0.0653 90.5 0.0654 68.6 (0.0647) 0.0602 $(6.40)^a$ 0.079 77Empty18 3 0.0656 79.6 (0.0669) 5.86 82 418 1.00 18 3 0.0656 83.9 (0.0669) 5.86 82418 1.00 18 3 0.0655 73.8 0.0156 0.66 0.66 83 a^277 7.43 42 3 0.0655 73.8 0.0156 0.66 0.68 $a^2Alumina$ 0.498 18 5 0.0652 59.1 0.0352 (4.39) 0.669 90Same18 3 0.0650 71.8 (0.0573) 4.30 (1.92) 90Same18 <t< td=""><td>58</td><td>927</td><td>7.43</td><td>42</td><td>3</td><td>0.0647</td><td>82.3</td><td>0.0068</td><td>(0.66)^a</td><td>0.083</td></t<>	58	927	7.43	42	3	0.0647	82.3	0.0068	(0.66) ^a	0.083
674181.001830.055440.10.07036.98069Empty1830.061291.691.691.691.691.691.6704181.001830.041134.80.0663 $(7.04)^a$ 071Same1830.061060.9 (0.0700) 6.4290.574Empty1830.060790.590.590.5754181.004230.055343.10.06146.5590.5764181.0011430.065390.590.590.590.5784181.004230.065947.70.0602 $(6.40)^a$ 90.7980Same1830.065679.6 (0.0644) 90.7090.580Same1830.065545.60.066537.0400.7981Same1830.065573.80.01560.660.66824181.001830.065573.80.01560.660.68839277.434230.065573.80.01560.660.6884a-Alumina0.6101830.065254.10.0352(4.39)090Same1830.065071.8(0.0573)4.30(1.92)929541.07183 </td <td>59</td> <td>Same</td> <td></td> <td>18</td> <td>3</td> <td>0.0651</td> <td>87.2</td> <td></td> <td>0.58</td> <td></td>	59	Same		18	3	0.0651	87.2		0.58	
69Empty183 0.0612 91.6 704181.00183 0.0411 34.8 0.0663 $(7.04)^a$ 0 71Same183 0.0610 60.9 (0.0700) 6.42 0 74Empty183 0.0607 90.5 0.0514 6.55 0 75418 1.00 423 0.0553 43.1 0.0614 6.55 0 76418 1.00 1143 0.0648 49.3 0.0548 6.29 0 77Empty18 3 0.0653 90.5 0.0548 6.29 0 78418 1.00 42 3 0.0659 47.7 0.0602 $(6.40)^a$ 0 79Same18 3 0.0656 79.6 (0.0644) 0.0669 5.86 82418 1.00 18 3 0.0655 45.6 0.06653 7.04 0 83927 7.43 42 3 0.0655 73.8 0.0156 0.66 0.688 $a-Alumina$ 0.610 18 3 0.0652 54.1 0.0444 4.39 1 89 $a-Alumina$ 0.498 18 5 0.0650 71.8 (0.0573) 4.30 (1.99) 90Same18 3 0.0640^b 23.9 0.0123 8.81 0.0123	67	418	1.00	18	3	0.0554	40.1	0.0703	6.98	0.606
704181.001830.041134.80.0663 $(7.04)^a$ 071Same1830.061060.9 (0.0700) 6.4274Empty1830.060790.5754181.004230.055343.10.06146.550764181.0011430.064849.30.05486.29077Empty1830.065390.577784181.004230.065947.70.0602 $(6.40)^a$ 079Same1830.065679.6 (0.0644) 6680Same1830.065545.60.06637.04081Same1830.065545.60.06637.040839277.434230.065573.80.01560.66088 α -Alumina0.6101830.065254.10.04444.39189 α -Alumina0.4981850.065071.8 (0.0573) 4.30(1929541.071830.0640 ^b 23.90.1238.810	69	Empty		18	3	0.0612	91.6			
71Same183 0.0610 60.9 (0.0700) 6.42 74Empty183 0.0607 90.5 90.5 75418 1.00 423 0.0553 43.1 0.0614 6.55 00 76418 1.00 1143 0.0648 49.3 0.0548 6.29 00 77Empty183 0.0653 90.5 0.0548 6.29 00 78418 1.00 423 0.0659 47.7 0.0602 $(6.40)^a$ 00 79Same183 0.0656 79.6 (0.0644) 0.0644 80Same183 0.0656 83.9 (0.0669) 5.86 82418 1.00 183 0.0655 45.6 0.06653 7.04 00 83927 7.43 42 3 0.0655 73.8 0.0156 0.66 0.68 84 α -Alumina 0.610 18 3 0.0652 54.1 0.0444 4.39 1.89 89 α -Alumina 0.498 18 5 0.0652 59.1 0.0352 (4.39) 00 90Same18 3 0.0660 71.8 (0.0573) 4.30 (1.92) 92954 1.07 18 3 0.0640^b 23.9 0.0123 8.81	70	418	1.00	18	3	0.0411	34.8	0.0663	(7.04) ^a	0.566
74Empty183 0.0607 90.5 75418 1.00 423 0.0553 43.1 0.0614 6.55 0 76418 1.00 1143 0.0648 49.3 0.0548 6.29 0 77Empty183 0.0653 90.5 0.578 418 1.00 42 3 0.0659 47.7 0.0602 $(6.40)^a$ 0 79Same18 3 0.0656 68.6 (0.0647) 0.0644 0.0656 0.0669 5.86 80Same18 3 0.0656 83.9 (0.0669) 5.86 0.6653 7.04 0.0633 81Same18 3 0.0655 45.6 0.0653 7.04 0.6633 0.666 0.6633 82418 1.00 18 3 0.0655 73.8 0.0156 0.666 0.6633 83927 7.43 42 3 0.0655 73.8 0.0156 0.666 0.6633 88 α -Alumina 0.610 18 3 0.0652 59.1 0.0352 (4.39) 0.996 90Same18 3 0.0650 71.8 (0.0573) 4.30 (1.992) 92954 1.07 18 3 0.0640^b 23.9 0.123 8.81	71	Same		18	3	0.0610	60.9	(0.0700)	6.42	
754181.004230.055343.10.06146.550764181.0011430.064849.30.05486.29077Empty1830.065390.590.590.590.590.590.5784181.004230.065468.6(0.0647)90.5 </td <td>74</td> <td>Empty</td> <td></td> <td>18</td> <td>3</td> <td>0.0607</td> <td>90.5</td> <td></td> <td></td> <td></td>	74	Empty		18	3	0.0607	90.5			
764181.0011430.064849.30.0548 6.29 077Empty1830.065390.590.590.590.590.5784181.004230.065947.70.0602 $(6.40)^{\alpha}$ 0079Same1830.065679.6 (0.0647) 90.580Same1830.065679.6 (0.0644) 90.581Same1830.065545.60.0669)5.86824181.001830.065545.60.06537.0400839277.434230.065573.80.01560.660088 α -Alumina0.6101830.065254.10.04444.39189 α -Alumina0.4981850.065071.8 (0.0573) 4.30(1929541.071830.0640 ^b 23.90.1238.810	75	418	1,00	42	3	0.0553	43.1	0.0614	6.55	0.564
77Empty183 0.0653 90.5 78418 1.00 423 0.0659 47.7 0.0602 $(6.40)^{a}$ 079Same183 0.0654 68.6 (0.0647) 080Same183 0.0656 79.6 (0.0644) 81Same183 0.0655 45.6 0.0669 5.8682418 1.00 183 0.0655 45.6 0.0653 7.040839277.43423 0.0655 73.8 0.0156 0.66 088 α -Alumina 0.610 183 0.0652 54.1 0.0444 4.39189 α -Alumina 0.498 185 0.0650 71.8 (0.0573) 4.30(192954 1.07 183 0.0640^{b} 239 0.123 881	76	418	1.00	114	3	0.0648	49.3	0.0548	6.29	0.524
78 418 1.00 42 3 0.0659 47.7 0.0602 $(6.40)^a$ 0 79 Same 18 3 0.0654 68.6 (0.0647) 0 80 Same 18 3 0.0656 79.6 (0.0644) 0 81 Same 18 3 0.0655 45.6 0.06633 7.04 0 82 418 1.00 18 3 0.0655 45.6 0.0653 7.04 0 83 927 7.43 42 3 0.0655 73.8 0.0156 0.66 0 88 α -Alumina 0.610 18 3 0.0652 54.1 0.0444 4.39 1 89 α -Alumina 0.498 18 5 0.0652 59.1 0.0352 (4.39) 0 90 Same 18 3 0.0650 71.8 (0.0573) 4.30 (1 92 954 1.07 18 3 0.0640 ^b 23.9 0.123 8.81 0	77	Empty		18	3	0.0653	90.5			
79Same183 0.0654 68.6 (0.0647) 80Same183 0.0656 79.6 (0.0644) 81Same183 0.0656 83.9 (0.0669) 5.86824181.00183 0.0655 45.6 0.0653 7.040839277.43423 0.0655 73.8 0.0156 0.66 088 α -Alumina0.610183 0.0652 54.1 0.0444 4.39189 α -Alumina0.498185 0.0650 71.8 (0.0573) 4.30(1929541.07183 0.0640^{b} 23.9 0.123 8.810	78	418	1.00	42	3	0.0659	47.7	0.0602	$(6.40)^{a}$	0.566
80Same183 0.0656 79.6 (0.0644) 81Same183 0.0656 83.9 (0.0669) 5.86 82418 1.00 183 0.0655 45.6 0.0653 7.04 0 83927 7.43 423 0.0655 73.8 0.0156 0.66 0 88 α -Alumina 0.610 183 0.0652 54.1 0.0444 4.39 1 89 α -Alumina 0.498 18 5 0.0652 59.1 0.0352 (4.39) 0 90Same183 0.0650 71.8 (0.0573) 4.30 (1.92) 92954 1.07 183 0.0640^{b} 23.9 0.123 8.81 0	79	Same		18	3	0.0654	68.6	(0.0647)		
81Same183 0.0656 83.9 (0.0669) 5.86 82418 1.00 183 0.0655 45.6 0.0653 7.04 0 83927 7.43 423 0.0655 73.8 0.0156 0.66 0 88 α -Alumina 0.610 183 0.0652 54.1 0.0444 4.39 1 89 α -Alumina 0.498 18 5 0.0652 59.1 0.0352 (4.39) 0 90Same183 0.0650 71.8 (0.0573) 4.30 $(1$ 92954 1.07 183 0.0640^{b} 23.9 0.123 8.81 0	80	Same		18	3	0.0656	79.6	(0.0644)		
824181.001830.065545.60.06537.040839277.434230.065573.80.01560.66088 α -Alumina0.6101830.065254.10.04444.39189 α -Alumina0.4981850.065259.10.0352(4.39)090Same1830.065071.8(0.0573)4.30(1929541.071830.0640 ^b 23.90.1238.810	81	Same		18	3	0.0656	83.9	(0.0669)	5.86	
839277.434230.065573.80.01560.66088 α -Alumina0.6101830.065254.10.04444.39189 α -Alumina0.4981850.065259.10.0352(4.39)090Same1830.065071.8(0.0573)4.30(1929541.071830.0640 ^b 2390.123881	82	418	1.00	18	3	0.0655	45.6	0.0653	7.04	0.558
88 α -Alumina0.6101830.065254.10.04444.39189 α -Alumina0.4981850.065259.10.0352(4.39)090Same1830.065071.8(0.0573)4.30(1929541.071830.0640 ^b 23.90.1238.810	83	927	7.43	42	3	0.0655	73.8	0.0156	0.66	0.186
89 α -Alumina0.4981850.065259.10.0352(4.39)090Same1830.065071.8(0.0573)4.30(1929541.071830.0640 ^b 23.90.1238.810	88	α-Alumina	0.610	18	3	0.0652	54.1	0.0444	4.39	1.00
90Same183 0.0650 71.8 (0.0573) 4.30 (1) 929541.07183 0.0640^b 239 0.123 881 0	89	α-Alumina	0.498	18	5	0.0652	59.1	0.0352	(4.39)	0.97
92 954 1.07 18 3 0.0640 ^b 23.9 0.123 8.81 0	90	Same		18	3	0.0650	71.8	(0.0573)	4.30	(1.60)
	92	954	1.07	18	3	0.0640	23.9	0.123	8.81	0.780

 TABLE 1

 Exchange with ¹⁸O Enriched Water (91.1% H₂¹⁸O) on Iron Catalysts and α-Alumina

^a These surface area values are assumed to be the same as those taken under identical conditions for Runs 83, 82, 57, and 54, respectively.

^b Due to an accident during this run, the $H_2^{16}O$ concentration, a_0 , was 70.3%. The figures for this catalyst are less certain, but as no more catalyst was available, the authors decided to report the values as shown.

by the mass spectrometer. As we know the amount, a_0 , and the ¹⁸O concentrations, x_0 , of the water added (¹⁸O concentration taken as that for a sample added to the empty reactor), we can calculate the amount of water, a_1 , exchangeable on the surface in the following way:

$$\frac{a_0 x_0}{a_0 + a_1} = x_1, \tag{1}$$

where x_1 is the concentration of ¹⁸O in the product out of the reactor.

The results of the experiments are shown in Table 1, together with a calculation from them of the number of O atoms/cm². Table 1 also gives the exchange on α -alumina (M88 and M89) of known surface area. For these, with exchange times of 3 and 5 hrs we found no significant difference in the exchangeable part of the sample, which came out close to 10¹⁵ atoms O/cm².

The question immediately arises as to whether the exchange carried out as described may reach oxygen atoms in the second and deeper layers of the alumina or the promoter molecules. Whalley and Winter (6) were able to show that $H_2^{18}O$ exchanged with the surface of Al_2O_3 at a very high rate whereas further exchange with interior oxygen was extremely slow even at 400°C. The first step in checking the depth of penetration of the exchange was to extend some of the equilibration times to 5 hr instead of the usual 3 hr. The results obtained as shown, for example, by Runs 50 and 89 in Table 1 indicated that the exchange was not appreciably greater in 5 hr than in 3 hr and was not, therefore, extending to lower layers of the promoters.

A more satisfactory way of ascertaining the penetration of the exchange to lower layers entailed exposing the samples to a stream of hydrogen for a period of 18 hr immediately after the first H₂¹⁸O exchange experiment. It is then possible to calculate from a second exchange experiment the amount of ¹⁶O from the second layer that has equilibrated with ¹⁸O atoms in the first layer from the exchange run. If such further exchange occurs, the ¹⁸O content of the surface layer will decrease from the value given for the equilibrated water from the first exchange down to a value, x'_1 . One can then calculate the value of x'_1 from the new exchange data by the equation

$$\frac{a_1 x'_1 + a_0 x_0}{a_0 + a_1} = x_2, \tag{2}$$

where a_1 is the number of milliatoms of oxygen calculated from the first exchange run as being present on the surface of the promoter, a_0 is the number of millimoles of ¹⁸O in the sample of H₂¹⁸O added for

the second run, and x_2 is the fraction of ¹⁸O in the product from the second equilibration. By this equation, calculations were made for a number of repeat runs as shown in Table 2. Runs 43-52 appeared to indicate that during the 18-hr exposure to a stream of hydrogen considerable oxygen-16 accumulated in the surface layer. This was found to be due, however, to water vapor contained to the extent of 4-8 ppm in the stream of hydrogen. The Δa_1 increments decreased to a very small value when, as in runs 56-81, the hydrogen passing over the iron catalysts came from the palladium-silver alloy diffusion tube. Apparently the oxygen diffusing into the first layer during these runs was only in the range 5-7% of the amount of oxygen in the surface of the iron or the promoters.

The experiments with aluminum oxide, however, indicated that in 18 hr considerable ¹⁶O diffused into and exchanged with ¹⁸O that was already in the first layer from the first exchange run. Thus, a comparison of Run 90 with Run 89 in Table 1 or Table 2 showed that additional oxygen-16 from the second layer equal to 60% of that originally in the first layer had equilibrated with the ¹⁸O from the first exchange experiment. In other words, during the 18-hr reduction 60% of the oxygen atoms from the second layer were equilibrated with the first layer of the alumina whereas only 5-7% of the lower lying oxygen atoms from the promoter on the iron catalysts so exchanged. This is consistent with the idea that the promoter molecules are present as single layers for the most part and do not therefore have many oxygen atoms in lower lying layers. Incidentally, it should be pointed out that the a_1 values for the iron catalysts in runs 43-52 indicate that most of the 4-8 ppm of water in the stream of hydrogen undergoes exchange with the ¹⁸O left on the promoter molecules during the first exchange run.

It is interesting to compare the results for different reduction times with respect to the total coverage of the surface with promoter oxygen, on the doubly promoted catalyst No. 418. Eighteen-hour reductions (Runs 43, 50, 51, 67, 70, and 82 in Table

M. No. ^b	Cat.	aı mAtom O on surface	Δa_1^a mAtom of oxygen	$\rm O/cm^{2} \times 10^{-1}$
43	418	0.0659		0.563
44	Same	(0.0835)	0.0177	
45	Same	(0.1038)	0.0203	
47	S(Fe)1	0.0067		0.040
48	Same	(0.0185)	0.0118	
51	418	0.0704		0.602
52	Same	(0.0830)	0.0126	
56	S(Fe)1	0.0009		0.012
57	Same	(0.0000)	0.0000	
70	418	0.0663		0.566
71	Same	0.0696	0.0033	
78	418	0.0602		0.566
79	Same	(0.0447)	0.0041	
80	Same	(0.0644)	-0.0003	
81	Same	(0.0667)	0.0025	
89	α-Alumina	0.0352		0.97
90	Same	(0.0573)	0.0221	

TABLE 2 Results of Consecutive Exchanges of H218O Enriched Water on Iron Catalysts and α -Alumina

 $a \Delta a_1$ is additional oxygen which seems to have equilibrated with surface oxygens during the 18-hr lapse between experiments.

^b In runs 43-52 tank hydrogen was used for reduction. It contained 4-8 ppm water vapor. For runs 56-90, the hydrogen was all diffused through a palladium-silver tube.

1) yield a value of 0.58×10^{15} oxygen atoms per cm². Forty-two-hour reductions (Runs 54 and 75) yield an average of $0.56\times 10^{\scriptscriptstyle 15}$ atoms of O per cm² and 114hour, yield (Run 76) 0.52×10^{15} . The percentage coverage with promoters thus decreases about 10%. Simultaneously, the total surface area changes from 7 m^2/g down to 6.3. Normally one would expect an increase in coverage of the surface with promoters as the iron crystals grow. Possibly, the observed effect is due to a partial clustering of the promoter molecules during the longer reduction period to form a multilayer of promoters in a few places. The same effect would be produced if there are a few low area crystallites of promoters present to which some of the disperse phase can gradually diffuse during longer periods of reduction.

Two other minor items should be noted in connection with the data in Table 1. For the pure iron catalyst S(Fe)1, 4% surface coverage with oxygen atoms was noted

in Run 47 when hydrogen gas was being used with 4-8 ppm of water vapor, whereas for hydrogen that had been allowed to diffuse through the Pd tube, the final coverage was only 1.2% (Run 56). The result is clearly in the expected direction even though the exact numerical values for the coverage are subject to considerable error. The final observation that may be worth noting is that the surface area for the sample of No. 418 reduced 114 hr (Run 76) was 6.3 m^2/g , whereas the area of the sample reduced 96 hr in Runs 79, 80, 81, and 82 with intervening exchange experiments with H₂¹⁸O had an area of only 5.86 m^2/g . This is in line with the usual expectation that exposing metallic iron to water vapor causes the iron crystals to grow.

In Table 3 are gathered the CO chemisorption data for some of the samples. The last column, "CO-coverage," is calculated using 16.2 Å² per CO molecule. The value given is, therefore, equal to $V_{\rm CO}/V_{\rm N2}$ where

M No.	Cat.	Cat. (g)	CO (mg)	m²/g	Number of CO molecules per cm ² \times 10 ⁻¹⁵	CO-cov.
52	418	0.652	0.54	6.54	0.27	0.44
54	418	0.705	0.52	6.40	0.25	0.40
57	S(Fe)1	0.713	0.46	1.98	0.70	1.13
59	927	0.703	0.12	0.58	0.65	1.05
75	418	0.643	0.50	6.55	0.25	0.41
76	418	0. 644	0.52	6.29	0.28	0.45
81	418	0.651	0.46	5.86	0.26	0.42
82	418	0.647	0.56	7.04	0.26	0.43
83	927	0.671	0.11	0.66	0.53	0.86
87	954	0.653	0.68	8.81	0.25	0.41
87^{b}	Same		0.63%			

 TABLE 3

 CO Chemisorption Measurements on Iron Catalysts

^a Assuming 16.2 Å²/CO, the coverage is equal to V_{CO}/V_{N_2} , where V_{N_2} is monolayer coverage of N₂ at -195.8°C and V_{CO} is the volume of adsorbed carbon monoxide.

^b After 1 hr pumping at -78° C.

Note: The sensitivity of the balance system used is about $\pm 5 \ \mu g$, giving an accuracy of about $\pm 5\%$ for M59 and M83, and about $\pm 1\%$ for the rest of the experiments.

 $V_{\rm CO}$ is the volume of carbon monoxide chemisorbed, and $V_{\rm N2}$ is the volume of physically adsorbed nitrogen required to form a monolayer at -195.8° C. In accordance with the theory that CO is chemisorbed only on the free iron of the surface, the area covered with CO and the one covered with oxygen containing species should give the total surface area. The values are certainly in the right direction even before one assumes specific sizes for the molecules involved. The values of $V_{\rm CO}/V_{\rm N_2}$ on a doubly promoted catalyst surface is, as we see, .400-.445 the highest

			$\mathbf{T}_{\mathbf{A}}$	ABLI	E 4				
COVERAGE	OF	CATALYS	r Suri	FACE	BY	PROMOTERS	AS	Judged	BY
Exchange with $H_2^{18}O$ and by CO Chemisorption									

		O Cov Area	erage by exch. a per Oatom	$1 - \theta_{\rm CO}$ Area per CO molecule		
Run M No.	Catalyst	12 Å ²	10 Å ²	16.2 Å ²	14.3 Å ²	
67	418	0.73	0.61			
70	418	0.69	0.57			
75	418	0.67	0.56	0.59	0,64	
70	418	0.62	0.52	0.55	0.60	
78	418	0.68	0.57			
81	418			0.58	0.63	
82	418	0.67	0.56	0.57	0.62	
58	927	0.099	0.083	-0.05	0.07	
83	927	0.23	0.186	0.14	0.24	
56	S(Fe)1		0.012	-0.13	0.00	
92	954		$0.78(0.62)^{a}$	0.59	0.64	
88	Al_2O_3		1.00			
89			0.97			

^a The value in parenthesis is for an area of 8 Å² per oxygen atom.



FIG. 3. The change in equilibrium concentrations in a sample exchanged four times with intervening reduction for 18 hr at 450°C with hydrogen, as a function of n, the number of introductions of the sample into the mass spectrometer.

value measured being the sample of 418 having the lowest oxygen number found (M76). The pure iron catalyst S(Fe)1 which has only 0.012×10^{15} O/cm² has a value of $V_{\rm CO}/V_{\rm N2} = 1.13$. Catalyst 927, which is unpromoted but assumed to contain about .15% Al₂O₃, seems to contain some inhomogeneities as M58 gave .083 $\times 10^{15}$ O/cm², while the sample for M83 gave .186 $\times 10^{15}$ O/cm². The CO chemisorption values, however, are in line with this as M59 (M58 exchanged with H₂O¹⁸ a second time) gave $V_{\rm CO}/V_{\rm N2} = 1.05$ and M83 gave 0.86.

In the above discussion and in Table 3 we have assumed that each oxygen atom on the promoter would occupy about 10 $Å^2$ and each CO molecule, 16.2 $Å^2$. Perhaps a little discussion and a few additional cross comparisons are in order.

The radius for oxygen ions in univalent crystals is, according to Pauling, 1.76 Å. This would correspond to a closest packing value of about 10.7 Å² per ion. For a promoter consisting of equal moles of K_2O and Al_2O_3 possibly as KAlO₂ a value of



FIG. 4. The change in adsorbed CO measured in a McBain balance on three different samples with pumping at -195.8° C as a function of time. At arrow, the surrounding temperature on M86 for catalyst No. 418 was increased to -78° C.

about 12 $Å^2$ per oxygen seems realistic. For CO the value 16.2 $Å^2$ is almost certainly too large.

Probably a better value for the area covered by a molecule of carbon monoxide would be one deduced from the ratio of 1.13 volume of carbon monoxide as a monolayer compared to the volume of a monolayer of physically adsorbed nitrogen. This would correspond to a figure of 14.3 $Å^2$ per CO. In Table 4, for comparison, the fraction of the surface covered by the promoter on the assumption of 10 $Å^2$ per oxygen ion and also 12 Å² are shown. Also are included the surface equivalent to $1-\theta_{co}$ where the coverage by carbon monoxide, $\theta_{\rm co}$ is calculated both from a value of 16.2 and a value of 14.3 Å² per CO molecule. It is evident that with a CO cross section of 14.3 Å² per molecule and an oxygen cross section of somewhere between 10 and 12 $Å^2$ excellent agreement is obtained for the fraction of the surface covered by promoters as judged by the oxygen-18 exchange work on the one hand and CO chemisorption on the other.

The result of catalyst 954, which is singly promoted with 10.2% Al₂O₃, is a bit uncertain because of an accident which occurred during the run (see footnote, Table 1) but the figure .78 \times 10¹⁵ O/cm² is probably right within a few percent. Considering the $V_{\rm CO}/V_{\rm N2}$ value of .41 found for this catalyst, one has to assign a smaller figure for each oxygen atom to obtain a coverage for the promoter on the surface agreeing with that deduced from the carbon monoxide chemisorption. In fact, a value of 8.2 Å² per oxygen atom would give a perfect fit.*

The amount of carbon monoxide chemisorbed needs to be discussed a bit further.

* Since only about 0.4% Al₂O₃ would be needed to cover 60% of the surface of catalyst 954, a considerable amount of the actual 10.2% Al₂O₃ must be located either on the inside of the crystallites or else in large crystals of Al₂O₃. The exact disposition of the large excess of the promoters is not, as yet, definitely known. As shown in Fig. 4, the amount adsorbed was essentially constant after about 2.5-3 hr pumping at -195.8°C. The pumping system was open and very effective such that the pressure reached after about 2.5 hr was about 10⁻⁶ mm Hg. If we now at this constant value change the temperature to -78° C, as done on M86, we get a steady decrease in the amount adsorbed of about 5-8% per hr. This is in agreement with Scholten's experiments (3). Scholten is obviously right when he stresses the importance of the design of the pumping system, the diameter of the tubes, etc. on the rate of desorption of chemisorbed CO at -78°C, and the difficulty in determining the time at which the pumping should be stopped. However, the suggestions made by Brunauer and Emmett (2) about using the value obtained after about 0.5 hr. pumping at -78°C probably in most cases will give a value for the volume of carbon monoxide chemisorbed within 5% of the right one. It seems, however, reasonable after these experiments that adsorption and pumping at -195.8°C gives a good value for the amount of chemisorbed CO provided one has a good pumping system with large diameter tubes. Pumping for 3-4 hr at -195°C should give a steadystate value for carbon monoxide chemisorption.

ACKNOWLEDGMENT

This project was made possible through the AEC grant # NYO-2008-7.

References

- 1. EMMETT, P. H., AND BRUNAUER, S. J. Am. Chem. Soc. 59, 310 (1937).
- BRUNAUER, S., AND EMMETT, P. H., J. Am. Chem. Soc. 62, 1732 (1940).
- SCHOLTEN, J. J. F., Thesis, Delft (The Netherlands) (1959).
- 4. EMMETT, P. H., AND GRAY, J., J. Am. Chem. Soc. 66, 1338 (1944).
- EMMETT, P. H., BRUNAUER, S., AND TELLER, E., J. Am. Chem. Soc. 60, 309 (1938).
- WHALLEY, E., AND WINTER, E. R. S., J. Chem. Soc. 1175 (1950).